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Erwin-Schrödinger Str. 44, D-67663 Kaiserslautern, Germany 4 A method for determining activity coefficients by molecular dynamics simulations is 5 presented. It is an extension of the OPAS method (osmotic pressure for the activity of 6 the solvent) developed in previous work for studying the solvent activity in electrolyte 7 solutions. That method is extended here to study activities of all components in 8 mixtures of molecular species. As an example, activity coefficients in liquid mixtures 9 of water and methanol are calculated for 298.15 K and 323.15 K at 1 bar using 10 molecular models from the literature. These dense and strongly interacting mixtures 11 pose a significant challenge to existing methods for determining activity coefficients 12 by molecular simulation. It is shown that the new method yields accurate results 13 for the activity coefficients which are in agreement with results obtained with a 14 thermodynamic integration technique. As the partial molar volumes are needed in 15 the proposed method, the molar excess volume of the system water + methanol is 16 also investigated. 17

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1 Activity Coefficients from Molecular Simulations using the OPAS Method

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18 I. INTRODUCTION

Chemical potentials or related properties like activities or activity coefficients are needed 19 for the determination of phase equilibria, and therefore their computation is a commonly en-20 countered task in molecular simulation studies. Most methods for determining the chemical 21 potential in molecular simulations are based on particle insertion. Often, the test particle 22 method of Widom¹ is used. However, in dense systems, that method tends to fail because of 23 extremely high energies upon insertion of the 'ghost' particles. To overcome this difficulty, 24 different elaborate sampling schemes have been suggested, e.g. the gradual insertion or ther-25 modynamic integration techniques^{2,3}. But still, for dense and strongly interacting systems, 26 long simulations are usually required, and method-specific simulation parameters have to be 27 determined by trial-and-error beforehand. Despite this, the methods may still turn out to 28 be unfeasible. 29

In this work, a new approach for obtaining activity coefficients in the liquid phase in molec-30 ular dynamics simulations is presented. It builds on previous work of our group in which the 31 OPAS method (osmotic pressure for the activity of the solvent) 4,5 was developed based on 32 ideas described by Murad and co-workers^{6–9}. In its previous version^{4,5}, the OPAS method 33 was developed for determining the solvent activity in electrolyte solutions. In the present 34 work, it is extended for determining activities of all species in mixtures of molecular species, 35 similar to the approach of Crozier and Rowley¹⁰. To demonstrate the feasibility and accu-36 racy of the new method, it is applied to determine activity coefficients in binary mixtures 37 of water and methanol at 298.15 K and 323.15 K and 1 bar. 38

³⁹ Binary mixtures of water and methanol have been the subject of many experimental and
⁴⁰ simulation studies. On the one hand, this is due to the importance of these substances

in many applications. On the other hand, as both water and methanol are strongly polar 41 and hydrogen bonding, their mixture has often been used as a test case for thermodynamic 42 models. The current version of the Dortmund Data Bank¹¹ lists more than 10,000 experi-43 mental data points for this system. Especially vapor-liquid equilibria and excess properties 44 have been studied by many groups in a wide range of conditions. Mixtures of water and 45 methanol have also been studied extensively using molecular simulation (e.g. in Refs. ^{10,12–41}). 46 In most of these studies, the structure of the solution is investigated. Some publications also 47 address hydrogen bonding statistics 12,13,18,28,29,38,41 , excess properties $^{18-21,27,33,34,36,38-41}$ and 48 transport properties^{16,18,21,22,32,39,41}. In contrast, the number of molecular simulation stud-49 ies of the vapor-liquid equilibrium or the related activity coefficients in the liquid phase is 50 small^{10,23,26,35}, due to the fact that these properties are difficult to compute accurately in 51 molecular simulations for dense liquid mixtures with strong interactions. Activity coefficients 52 are derivatives of the free energy, so that they cannot be obtained by standard sampling 53 and instead, special algorithms have to be designed for their calculation. As outlined above, 54 most of the common algorithms to do so are based on particle insertions, which become very 55 cumbersome for systems of strongly interacting particles. 56

In the present work, it is shown that the proposed extension of the OPAS method enables an accurate calculation of activity coefficients, even in challenging mixtures such as water + methanol. Since partial molar volumes are needed in the evaluation of the OPAS simulation results, the molar excess volume of the mixture is also investigated. To demonstrate the viability of the extended OPAS approach, we compare its results to results obtained with a thermodynamic integration technique.
The paper is structured as follows: In Section II, we briefly describe the employed molecular

⁶⁴ models. The rest of Section II is devoted to the derivation and presentation of the exten-

⁶⁵ sion of the OPAS approach. This includes a procedure for obtaining partial molar volumes.
⁶⁶ In Section III, these volumetric properties are discussed first. Then, the OPAS simulation
⁶⁷ results are presented and compared to the results from thermodynamic integration, before
⁶⁸ we conclude in Section IV.

⁶⁹ II. MOLECULAR MODELS AND SIMULATION METHODS

70 A. Molecular Models

In the present study, the TIP4P/2005 water model⁴² and a methanol model from previous work of our group⁴³ are used. Both are known to give good predictions of pure component properties. Both models are rigid and non-polarizable and consist of Lennard-Jones (LJ) sites and partial charges. The potential is therefore

$$U = U_{\rm LJ} + U_{\rm CC} = \sum_{i=1}^{N-1} \sum_{j=i+1}^{N} \left\{ \sum_{a=1}^{n_i^{\rm LJ}} \sum_{b=1}^{n_j^{\rm LJ}} 4\epsilon_{ijab} \left[\left(\frac{\sigma_{ijab}}{r_{ijab}} \right)^{12} - \left(\frac{\sigma_{ijab}}{r_{ijab}} \right)^6 \right] + \sum_{c=1}^{n_i^e} \sum_{d=1}^{n_j^e} \frac{1}{4\pi\varepsilon_0} \frac{q_{ic}q_{jd}}{r_{ijcd}} \right\}.$$
 (1)

⁷⁵ Here, a, b, c and d denote sites, i and j denote molecules, ε_0 is the vacuum permittivity, ⁷⁶ ϵ_{ijab} and σ_{ijab} are the Lennard-Jones energy and size parameters, r_{ijab} and r_{ijcd} are site-site ⁷⁷ distances, and q_{ic} and q_{jd} are the magnitudes of the partial charges.

⁷⁸ To describe the interaction between unlike LJ sites, the Lorentz-Berthelot combining rules⁷⁹ are used:

$$\sigma_{ijab} = \frac{\sigma_{iiaa} + \sigma_{jjbb}}{2},\tag{2}$$

$$\epsilon_{ijab} = \sqrt{\epsilon_{iiaa}} \epsilon_{jjbb}.$$
 (3)

⁸⁰ B. Computation of Activity Coefficients with the OPAS Method

The OPAS method was developed in previous work with the aim of computing activities in electrolyte solutions. It is only introduced briefly here, for details, the reader is referred to our previous publications^{4,5}.

⁸⁴ OPAS simulations are molecular dynamics simulations of the osmotic equilibrium between ⁸⁵ a pure component phase (') and a mixture phase (") which are in contact via a virtual ⁸⁶ semipermeable membrane. There is only one permeable component *i*. The membrane is ⁸⁷ realized in the simulation by applying an external force field on all molecules but those of ⁸⁸ component *i* to keep them inside the mixture phase ("), so that the phase (') contains pure *i*. ⁸⁹ The osmotic pressure Π , which is the pressure difference between the two phases, is sampled ⁸⁰ as the membrane force per area.

In OPAS simulations, the temperature T and the pressure p' of the pure component phase are specified. The simulation results are the osmotic pressure Π and the composition of the mixture phase \underline{x} . The goal is the computation of the activity coefficient $\gamma_i(T, p', \underline{x})$ of the permeable component i at the specified temperature T and pressure p' as well as the composition of the mixture phase x.

In the following, it is shown how $\gamma_i(T, p', \underline{x})$ is obtained. Normalizing the chemical potentials according to Raoult and rearranging the equilibrium condition for the osmotic equilibrium described above yields

$$\mu_i^{\text{pure}}(T, p'') - \mu_i^{\text{pure}}(T, p') = -RT \ln a_i(T, p'', \underline{x}).$$
(4)

⁹⁹ Herein, μ_i and a_i are the chemical potential and activity of the permeable component *i*, and ¹⁰⁰ *R* is the universal gas constant. Combining Eq. (4) with

$$\mu_i(T, p', \underline{x}) = \mu_i^{\text{pure}}(T, p') + RT \ln a_i(T, p', \underline{x})$$
(5)

$$\mu_i(T, p'', \underline{x}) = \mu_i^{\text{pure}}(T, p'') + RT \ln a_i(T, p'', \underline{x})$$
(6)

yields

$$\mu_i(T, p'', \underline{x}) - \mu_i(T, p', \underline{x}) = -RT \ln a_i(T, p', \underline{x}).$$
(7)

Using $\Pi = p'' - p'$ this leads to

$$\int_{p'}^{p'+\Pi} v_i(T, p, \underline{x}) \, dp = -RT \ln a_i(T, p', \underline{x}). \tag{8}$$

Splitting the activity a_i into the mole fraction x_i and the activity coefficient γ_i finally yields the desired relation

$$\ln \gamma_i(T, p', \underline{x}) = -\frac{1}{RT} \int_{p'}^{p' + \Pi} v_i(T, p, \underline{x}) \, dp - \ln x_i.$$
(9)

In Eq. (9), T and p' are specified, and Π and x_i are OPAS simulation results. Additionally, the partial molar volume $v_i(T, p, \underline{x})$ is needed for the determination of the activity coefficient, and an integration over the pressure has to be carried out. In the present work, v_i was determined from the molar excess volume $v^{\rm E}$ as described in Section II C.

The relation between the activity and the osmotic pressure, cf. Eq. (9) has also been exploited in a recent paper by Smith et al.⁴⁴. They, however, proceed in the opposite direction: A relation similar to Eq. (9) is employed to calculate the osmotic pressure in an electrolyte solution from knowledge of the solvent activity.

To obtain the N activity coefficients in a mixture of N components, N independent OPAS simulation runs have to be carried out. In each run, a different component i is treated as the permeable component, while all others cannot permeate the membrane. By the present method, the mixture phase composition \underline{x} is not specified directly. Rather, the composition ¹¹³ is a simulation result. However, the initial conditions of the run can generally be chosen ¹¹⁴ such that the final result for the composition is close to any desired value. The OPAS ¹¹⁵ simulation runs are extremely simple, fast and robust compared to simulations employing ¹¹⁶ particle insertion methods.

¹¹⁷ C. Computation of Molar Excess Volumes

The molar excess volume $v^{\rm E}$ of a mixture of N components is defined as:

$$v^{\mathrm{E}} = v - \sum_{i=1}^{N} x_i v_i^{\mathrm{pure}},\tag{10}$$

where v is the molar volume of the mixture and v_i^{pure} are the pure component molar volumes. The molar excess volume is a function of temperature, pressure and composition: $v^{\text{E}} = v^{\text{E}}(T, p, \underline{x})$. In the present work, only binary mixtures of two components i and j are studied, so that Eq. (10) becomes

$$v^{\mathrm{E}} = v - x_i v_i^{\mathrm{pure}} - x_j v_j^{\mathrm{pure}}.$$
(11)

The molar excess volume is computed here by performing a series of simulations at different compositions in the NpT ensemble and applying Eq. (11). As the osmotic pressures obtained in OPAS simulations can reach very high values, cf. Section III B, such simulations are carried out at several isobars up to elevated pressures. For each isobar, the molar excess volumes can be correlated by a Redlich-Kister type expression:

$$v^{\rm E} = x_i x_j \left(A_0 + \sum_k A_k (x_i - x_j)^k \right), \ k = 1, 2, \dots,$$
 (12)

where A_0 and the A_k are fitting parameters. Adjusting Eq. (12) to the NpT simulation results is a standard polynomial regression. From that correlation, the partial molar volume v_i of component *i* can be obtained as

$$v_{i} = \left(\frac{\partial V}{\partial n_{i}}\right)_{T,p,n_{j\neq i}} = v_{i}^{\text{pure}} + v^{\text{E}} + x_{j} \left(\frac{\partial v^{\text{E}}}{\partial x_{i}}\right)_{T,p,n_{j\neq i}}$$
(13)

where

$$\left(\frac{\partial v^{\mathrm{E}}}{\partial x_{i}}\right)_{T,p,n_{j\neq i}} = (x_{j} - x_{i}) \left(A_{0} + \sum_{k} A_{k}(x_{i} - x_{j})^{k}\right) + 2x_{i}x_{j} \left(\sum_{k} A_{k}k(x_{i} - x_{j})^{(k-1)}\right), \ k = 1, 2, \dots .$$
(14)

¹²⁶ D. Details on the Simulations in the System Water + Methanol

In the present study, binary mixtures of water and methanol were considered. The aim 127 was to determine activity coefficients at p' = 1 bar and either T = 298.15 K or T = 323.15 K 128 over a wide concentration range. Details of the OPAS simulations and the standard NpT129 simulations for obtaining molar excess volumes are given in the Appendices A1 and A2, 130 respectively. To validate the results for the activity coefficients determined with the OPAS 131 method, they were also determined from independent simulations employing a thermody-132 namic integration technique^{3,45}. Technical details of these simulations are given in Appendix 133 АЗ. 134

135 III. RESULTS AND DISCUSSION

Simulation results of the NpT simulations for obtaining the molar excess volumes are given in Table I, and the OPAS simulation results are given in Table II. Table III contains the results of the simulations using thermodynamic integration to validate our OPAS computations. In all tables, numbers in parentheses indicate the simulation uncertainties in the last given digit. The uncertainties for $v^{\rm E}$ were determined from error propagation of the simulation results for ρ via Eq. (11). The uncertainties in the evaluation of γ_i from the OPAS results were then estimated by using the simulation results for $v^{\rm E}$ disturbed by their uncertainties in the correlation fitting, cf. Eq. (12), combined with error propagation of the uncertainty of II. The uncertainties in the evaluation of γ_i from the simulations employing thermodynamic integration were estimated by error propagation of the simulation results for $\tilde{\mu}_i$, cf. Eq. (A2) in Appendix A 3.

Since the focus of the present work is to demonstrate the viability of the OPAS method, we
discuss the comparison of the model predictions to experimental data only briefly.

¹⁴⁹ A. Molar Excess Volumes and Partial Molar Volumes

First, the molar excess volumes of binary mixtures of water and methanol are discussed. 150 The molecular simulation results are compared to correlations of experimental data for the 151 two temperatures studied here in Fig. 1. The results of the predictive simulations with the 152 Lorentz-Berthelot rules capture the trends of the experimental data reasonably. The location 153 of the minimum in $v^{\rm E}$ at approximately equimolar composition is predicted correctly, how-154 ever, its magnitude is underestimated by about 20%. The experimental data show that the 155 difference between the two temperatures is almost negligible, and the molecular simulation 156 results also capture this feature well. Quantitative agreement with the experimental data 157 can probably be achieved by introducing an adjustable parameter in the mixing rules^{20,27}. 158 In the present work, however, our main concern is demonstrating the viability of the OPAS 159 method for computing activity coefficients, and quantitative agreement with the experimen-160 tal data is less important, so that we refrain from fitting binary interaction parameters. 161 Similar simulations were carried out at higher pressures. The simulation data were described 162

¹⁶³ by Redlich-Kister correlations, cf. Eq. (12). The results are shown in Fig. 2, the fit param-¹⁶⁴ eters are reported in Table I. Up to pressures of about p = 10 MPa, the pressure effect on

the partial molar volumes is small, but it becomes increasingly important at the elevated 165 pressures. There, the partial molar volumes of both water and methanol exhibit a maxi-166 mum. Comparing the two different temperatures, the curves are qualitatively similar. The 167 main difference is a vertical shift of the curves resulting from the temperature dependence 168 of the pure component molar volumes, which are in good agreement with the molar volumes 160 computed from equations of state for both studied temperatures, cf. Fig. 2. A more detailed 170 comparison of the partial molar volumes obtained from the simulations to experimental data 171 is presented in the Supplementary Material. 172

173 B. Osmotic Pressures and Activity Coefficients

The osmotic pressures obtained by OPAS simulations at the two studied temperatures, 174 using either water or methanol as the permeable component, are shown in Fig. 3. Simula-175 tions were carried out here for mole fractions above about 0.1 of the permeable component i176 in the mixture phase. At lower mole fractions of the permeable component, the statistics for 177 the undisturbed mixture phase becomes poor for the present scenario. Fig. 3 shows that the 178 osmotic pressure rises to very high values at low concentrations of the permeable component. 179 Comparing the simulation results at the two temperatures shows that the temperature de-180 pendence of the osmotic pressures is very small. When evaluating activity coefficients from 181 the OPAS simulations, the osmotic pressures are the upper bounds for the integration over 182 the pressure in Eq. (9). 183

In order to evaluate the OPAS simulations to get activity coefficients, the partial molar volume of the respective permeable component was evaluated analytically at the composition of interest from the Redlich-Kister type correlations presented in Fig. 2. The resulting series of values at different pressures $v_i(p)$ was then fit to a polynomial of second degree.

This polynomial was integrated over the pressure in order to obtain the activity coefficients 188 according to Eq. (9). The results are shown in Fig. 4 for both studied temperatures. The 189 error bars for the activity coefficient obtained with the OPAS method are within symbol 190 size. The OPAS data are smooth for both temperatures, and in the Supplementary Material, 191 it is shown that the numbers for $\gamma_{\rm W}$ and $\gamma_{\rm MeOH}$ obtained from independent OPAS simula-192 tions are thermodynamically consistent. For T = 323.15 K, activity coefficients were also 193 determined from sampling the chemical potential by thermodynamic integration in NpT194 simulations. The results are presented in Fig. 4, right panel, and in Table III. The data 195 obtained by thermodynamic integration scatter much more strongly than those from the 196 OPAS method, even though very long simulations were carried out, cf. Appendix A 3. At 197 T = 298.15 K, thermodynamic integration breaks down due to the increased density. In 198 contrast, the increased density at low temperatures has no effect on the performance of the 199 OPAS method. Taking into account the uncertainties in the results obtained from thermo-200 dynamic integration, both simulation techniques agree well. 201

The data obtained from the investigated models qualitatively agree with the experimental results. However, together with the original Lorentz-Berthelot rules these models are not able to predict the activity coefficients quantitatively. Improvements could be achieved by parameter fitting, which is beyond the scope of the present work.

206 IV. CONCLUSIONS

An extension of the OPAS method is presented. It is based on the simulation of an osmotic equilibrium and enables accurate calculations of activity coefficients even in dense, strongly interacting mixtures. For every component i in the mixture, a set of OPAS simulations has to be carried out treating that component i as the permeable one. In the simulations,

the temperature T and the pressure p' in the pure component phase are specified and the 211 activity coefficient γ_i at the composition of the mixture phase and at T and p' is determined. 212 As high osmotic pressures are obtained, especially in simulations at high dilution of the 213 respective permeable component, the pressure dependence of the activity coefficients has to 214 be taken into account, so that the partial molar volume v_i of component i in the mixture 215 has to be known. It is obtained here from simple and inexpensive NpT simulations. The 216 proposed procedure yields activity coefficients with low uncertainty and is very robust. It is 217 an advantage of the method that its efficiency does not depend on the studied statepoint, so 218 that it is applicable to systems of low temperature and high density without modifications. 219 Furthermore, it may also be applied to solutions of polymers or proteins, for which algorithms 220 based on particle insertion become very tedious. Using OPAS simulations, the activity of the 221 solvent can be determined with high accuracy. The activity of the solute is then available 222 from the Gibbs-Duhem equation, an approach applied successfully in our previous work on 223 electrolyte solutions. 224

225 SUPPLEMENTARY MATERIAL

The supplementary material contains a comparison of the partial molar volumes from molecular simulation and experiment as well as a consistency check of the activity coefficients determined from independent OPAS simulation runs.

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²³⁸ Appendix A: Simulation Details

All simulations of the present work were carried out with an extended version of the 230 molecular simulation program $ms2^{46}$. All simulations employed the velocity scaling ther-240 mostat, and electrostatic long-range interactions were calculated using the reaction field 241 method^{47,48} with tinfoil boundary conditions. In all simulations, the electrostatic cutoff ra-242 dius was equal to the Lennard-Jones cutoff radius of 15 Å. In all molecular dynamics (MD) 243 simulations, the time step was 1.2 fs, and the pressure was kept constant in MD NpT simu-244 lations using Andersen's barostat. Statistical simulation uncertainties were estimated with 245 the block average method by Flyvbjerg and Petersen⁴⁹. 246

247 1. OPAS Simulations

OPAS MD simulations were carried out as in previous work^{4,5}, using 4000 particles. At first, simulations in a modified NpT ensemble were carried out, in which equilibration and production took 2,000,000 and 5,000,000 time steps, respectively. The resulting box volume V was then used for a run in the NVT ensemble, in which equilibration and production took 2,000,000 and 10,000,000 time steps, respectively.

253 2. Simulations for Molar Excess Volumes

Conventional MD simulations were carried out in the NpT ensemble with 1000 particles. Equilibration and production took 100,000 and 2,000,000 time steps, respectively.

256 3. Simulations using Thermodynamic Integration

The chemical potential of both components was sampled with thermodynamic integration in Monte Carlo (MC) simulations in the NpT ensemble with 1000 particles, employing an adaptive sampling technique with non-linear scaling as proposed by Kristóf and Rutkai⁴⁵ (using 100 bins from $0.2 \le \lambda \le 1$, with a maximum λ displacement per attempt of 0.1 and the exponent d = 4). These simulations yield the reduced residual chemical potential

$$\tilde{\mu}_i = [\mu_i - \mu_i^{\rm id}(T)]/(RT),\tag{A1}$$

where $\mu_i^{id}(T)$ is the part of the ideal chemical potential of component *i* that only depends on temperature. Activity coefficients are obtained from

$$\ln \gamma_i = \tilde{\mu}_i - \tilde{\mu}_i^{\text{pure}} - \ln x_i. \tag{A2}$$

The fluid was equilibrated for 50,000 MC loops, before sampling was carried out for 9,600,000 MC loops. Each MC loop consisted of $N_{\rm NDF}/3$ steps, where $N_{\rm NDF}$ indicates the total number of mechanical degrees of freedom of the system, plus one attempt to resize the box according to the Metropolis acceptance criterion.

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397 FIGURES



FIG. 1. Molar excess volume of water-methanol mixtures at p = 1 bar. Open circles show results from predictive molecular simulations, dotted lines show a Redlich-Kister correlation to these results. Statistical uncertainties are within symbol size. The solid lines are correlations to experimental data by Coquelet et al.⁵⁰.



FIG. 2. Partial molar volumes of water (top) and methanol (bottom) in water-methanol mixtures obtained from Redlich-Kister correlations fit to molecular simulation results for the molar excess volumes. Colored lines correspond to different pressures (from top to bottom): (-) p = 0.1 MPa, (-) p = 10 MPa, (-) p = 50 MPa, (-) p = 100 MPa, (-) p = 300 MPa. The open squares colored accordingly are molar volumes of pure water and pure methanol computed from the equations of state by Wagner and Pruss⁵¹ and by de Reuck and Craven⁵², respectively.



FIG. 3. Osmotic pressures obtained in OPAS simulations using water as the permeable component
(blue) or methanol as the permeable component (red), dotted lines are guides to the eye. Statistical
uncertainties are within symbol size.



FIG. 4. Activity coefficients of methanol (red) and water (blue) in water-methanol mixtures at p = 1 bar. The open circles show simulation results obtained with the OPAS method. Statistical uncertainties of the OPAS simulation results are within symbol size. In the right panel, the open squares show simulation results using the same molecular models, but obtained from sampling the chemical potential with thermodynamic integration. Solid lines show NRTL fits to the experimental data of Kooner et al.⁵³ (left panel) and by Bernatova et al.⁵⁴ (right panel).

TABLES

		$\rho(T=2$	298.15 K) /	T = 298.15 K				
	$x_{\rm MeOH} \ / \ { m mol} \ { m mol}^{-1}$					Parameters for $v^{\rm E}$ / cm ³ mol ⁻¹		
p / MPa	0	0.25	0.5	0.75	1	A_0	A_1	A_2
0.1	55.21(1)	43.16(1)	34.92(1)	28.968(6)	24.519(4)	-3.2292	-0.0916	0.0372
10	55.48(1)	43.384(9)	35.126(8)	29.203(6)	24.766(5)	-2.9315	-0.0829	-0.1153
50	56.47(1)	44.149(9)	35.907(6)	30.021(5)	25.602(4)	-2.1386	0.0819	-0.0695
100	57.59(1)	45.012(8)	36.757(6)	30.850(5)	26.417(3)	-1.6183	0.2426	0.1887
300	61.194(8)	47.756(6)	39.197(5)	33.136(4)	28.600(2)	-0.5657	0.3927	0.2493
		$\rho(T=3)$	323.15 K) /	mol l^{-1}	<u> </u>		T = 323.15	K
		$\rho(T = 3)$ x_{Me0}	23.15 К) / _{ОН} / mol n	mol l^{-1}		7 Parameter	T = 323.15 T	$ m K$ $ m cm^3~mol^{-1}$
 <i>p</i> / MPa	0	$\rho(T = 3$ x_{Me0} 0.25	23.15 К) / _{Эн} / mol n 0.5	$\frac{1}{1} \mod 1^{-1}$ 0.75	1	Paramete A_0	$T = 323.15$ rs for $v^{\rm E}$ / o A_1	K $cm^3 mol^{-1}$ A_2
 p / MPa 0.1	0 54.69(1)	$ \rho(T = 3) $ x_{Me0} 0.25 42.259(9)	23.15 K) / DH / mol n 0.5 33.973(7)	$\frac{1}{100} = \frac{1}{100} = \frac{1}$	1 23.758(5)	Parameter A_0 -3.0137	T = 323.15 rs for $v^{\rm E} / c$ A_1 0.0507	$ \begin{array}{c} \text{K}\\ \text{Cm}^3 \text{ mol}^{-1}\\ \hline A_2\\ -0.2649\\ \end{array} $
<i>p</i> / MPa 0.1 10	$0 \\ 54.69(1) \\ 54.93(1)$	$\rho(T = 3)$ x_{Me0} 0.25 42.259(9) 42.517(8)	223.15 K) / _{DH} / mol n 0.5 33.973(7) 34.228(8)	$\begin{array}{c} \begin{array}{c} & & \\ $	1 23.758(5) 24.048(4)	$ \begin{array}{c} 7 \\ Parameter \\ \hline A_0 \\ -3.0137 \\ -2.7153 \\ \end{array} $	T = 323.15 rs for $v^{\rm E} / c$ A_1 0.0507 -0.0796	K $m^3 \text{ mol}^{-1}$ A_2 -0.2649 -0.2904
<i>p</i> / MPa 0.1 10 50	$\begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$\rho(T = 3)$ x_{Me0} 0.25 $42.259(9)$ $42.517(8)$ $43.378(7)$	223.15 K) / DH / mol n 0.5 33.973(7) 34.228(8) 35.138(6)	$\begin{array}{c} & \text{mol } 1^{-1} \\ & \text{nol}^{-1} \\ & 0.75 \\ & 28.123(6) \\ & 28.390(5) \\ & 29.310(4) \end{array}$	1 23.758(5) 24.048(4) 24.989(3)	$\begin{array}{c} & & & & & & \\ & & & & \\ & & & & & \\$	F = 323.15 rs for $v^{\rm E} / c$ A_1 0.0507 -0.0796 -0.0070	K A_2 -0.2649 -0.2904 0.0629
<i>p</i> / MPa 0.1 10 50 100	$\begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$\rho(T = 3)$ x_{Me6} 0.25 $42.259(9)$ $42.517(8)$ $43.378(7)$ $44.314(6)$	223.15 K) / DH / mol n 0.5 33.973(7) 34.228(8) 35.138(6) 36.047(5)	$\begin{array}{c} & \text{mol } 1^{-1} \\ & \text{nol}^{-1} \\ \hline 0.75 \\ 28.123(6) \\ 28.390(5) \\ 29.310(4) \\ 30.205(4) \end{array}$	1 23.758(5) 24.048(4) 24.989(3) 25.862(3)	$\begin{array}{c} & & & & & \\ & & & &$	F = 323.15 rs for v^{E} / c A_{1} 0.0507 -0.0796 -0.0070 0.1003	K $m^3 \text{ mol}^{-1}$ A_2 -0.2649 -0.2904 0.0629 0.0757

TABLE I. Densities and parameters of Redlich-Kister correlations, cf. Eq. (12), fit to molar excess
volumes for binary mixtures of water and methanol.

T = 1	298.15 K		T = 323.15 K			
$x_{\rm MeOH} / {\rm mol \ mol^{-1}}$	Π / MPa	$\gamma_{ m MeOH}$	$x_{\rm MeOH} / {\rm mol \ mol^{-1}}$	Π / MPa	$\gamma_{ m MeOH}$	
0.2163(5)	60.6(3)	1.84(1)	0.2192(6)	62.5(3)	1.84(1)	
0.3484(5)	45.7(3)	1.407(6)	0.3525(5)	46.4(2)	1.42(6)	
0.4907(5)	33.4(2)	1.198(4)	0.4919(4)	34.2(2)	1.212(4)	
0.6442(2)	23.3(2)	1.067(3)	0.6463(2)	23.9(1)	1.072(2)	
0.8126(1)	12.1(1)	1.009(2)	0.8129(1)	12.4(1)	1.014(2)	
0.9605(1)	2.382(5)	1.0011(8)	0.9606(1)	2.33(5)	1.0039(8)	
$x_{\rm MeOH} \ / \ {\rm mol} \ {\rm mol}^{-1}$	П / MPa	$\gamma_{ m W}$	$x_{\rm MeOH}$ / mol mol ⁻¹	Π / MPa	$\gamma_{\rm W}$	
0.8779(8)	218.0(5)	2.18(1)	0.8862(8)	224.1(5)	2.46(1)	
0.7901(8)	140.9(4)	1.946(7)	0.7866(8)	151.0(5)	1.896(7)	
0.5098(7)	56.9(4)	1.376(4)	0.5159(7)	58.9(3)	1.410(3)	
0.2235(4)	25.8(2)	1.069(2)	0.2262(4)	26.0(2)	1.085(2)	
0.0407(1)	5.36(9)	1.0025(7)	0.0408(1)	5.72(9)	1.0028(7)	

TABLE II. Results of OPAS simulations and deduced activity coefficients. The upper block shows

results of simulations with methanol as the permeable component, the lower block shows results of

428 simulations with water as the permeable component.

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429 TABLE III. Reduced residual chemical potentials and activity coefficients of water and methanol

$x_{\rm MeOH} / {\rm mol \ mol^{-1}}$	$ ilde{\mu}_{ m MeOH}$	$ ilde{\mu}_{ m W}$	$\gamma_{ m MeOH}$	$\gamma_{ m W}$
0	_	-10.40(6)	_	1
0.2	-8.68(6)	-10.60(7)	1.9(1)	1.03(7)
0.4	-8.20(6)	-10.72(8)	1.5(1)	1.22(9)
0.6	-8.05(6)	-10.79(9)	1.18(7)	1.7(1)
0.8	-7.92(6)	-11.44(8)	1.01(6)	1.8(1)
1	-7.71(6)	_	1	_

430 <u>at T = 323.15 K and p = 1 bar obtained from thermodynamic integration.</u>

Supplementary Material to:

Activity Coefficients from Molecular Simulations using the OPAS Method Maximilian Kohns, Martin Horsch, and Hans Hasse

1 Comparison of Partial Molar Volume Results to Experimental Data In the literature, two sets of experimental data on densities or molar excess volumes of mixtures of water and methanol at elevated pressures exist: Safarov et al. [1] studied the system at pressures up to p = 60 MPa and report data for T = 298.15 K and T = 323.15 K. Yokoyama et al. [2] studied the system at pressures up to p = 200 MPa, but report data only at T = 320 K and higher temperatures. However, T = 320 K seems close enough to T = 323.15 K to enable at least a qualitative comparison with our molecular simulation predictions. Both groups only give numbers for the densities or molar volumes, respectively.

Both groups only give numbers for the densities or molar volumes, respectively. Thus, they were correlated with a Redlich-Kister approach, similar to the treatment of the molecular simulation data discussed in the main text, and the partial molar volumes were computed from these correlations. To enable this, the data of Safarov et al. [1] were complemented with the pure component molar volumes computed from the equations of state by Wagner and Pruss [3] for water and de Reuck and Craven [4] for methanol, respectively. Yokoyama et al. [2] report data for pure methanol, which were used here, and their data set was also complemented with the equation of state of Wagner and Pruss [3] for water. The partial molar volumes obtained in this manner are shown in Figs. S1 and S2, respectively, where they are compared to the predictions from molecular simulations already discussed in the main text.



Figure S1: Partial molar volumes of water (top) and methanol (bottom) in watermethanol mixtures obtained from Redlich-Kister correlations. Solid lines: fit to molecular simulation results for the molar excess volumes. Dashed lines: Fit to experimental data by Safarov et al. [1]. Colors correspond to different pressures (from top to bottom): (-) p = 0.1 MPa, (-) p = 10 MPa, (-) p = 50 MPa.



Figure S2: Partial molar volumes of water (top) and methanol (bottom) in water-methanol mixtures obtained from Redlich-Kister correlations. Solid lines: fit to molecular simulation results for the molar excess volumes, T = 323.15 K. Dashed lines: Fit to experimental data by Yokoyama et al. [2], T = 320 K. Colors correspond to different pressures (from top to bottom):
(-) p = 0.1 MPa, (-) p = 10 MPa, (-) p = 50 MPa, (-) p = 100 MPa.

The molecular simulation predictions of v_{MeOH} (bottom panels in both figures) compare favorably with both sets of experimental data. The qualitative dependence of v_{MeOH} on x_{MeOH} is predicted correctly. This is true for all isobars. However, the molecular simulation predictions show a quantitative offset from the experimental data, which mainly arises from the differences in v_{MeOH}^{pure} already discussed in the main text. Additionally, the partial molar volume of methanol at infinite dilution in water v_{MeOH}^{∞} seems to be slightly underpredicted. Regarding $v_{\rm W}$ (top panels in both figures), the agreement between the molecular simulation predictions and the experimental data is very good in the water-rich region. In the methanol-rich region, however, the two sets of experimental data disagree. It is therefore difficult to assess the molecular simulation predictions. If compared to the experimental data of Safarov et al. [1] (Fig. S1), the numbers for the partial molar volume of water at infinite dilution in methanol $v_{\rm W}^{\infty}$ are predicted correctly, but the dependence of $v_{\rm W}$ on $x_{\rm MeOH}$ is not depicted correctly. If compared to the experimental data of Yokoyama et al. [2] (Fig. S2), the prediction of the trend is very good, whereas the numbers found for $v_{\rm MeOH}^{\infty}$ are too low. Altogether, taking into account that the employed molecular models are conceptually simple and no adjustment to experimental data of the binary system was made, the predictions of the partial molar volumes are quite satisfactory.

2 NRTL Fit to Simulation Results

In order to check the thermodynamic consistency of the values for γ_{W} and γ_{MeOH} obtained from independent OPAS simulation runs, an NRTL model was fit to the data, cf. Fig. S3. For both temperatures, the data and the fits agree well, which shows the consistency of the OPAS simulation results.



Figure S3: Activity coefficients of methanol (red) and water (blue) in water-methanol mixtures at p = 1 bar. The open circles show simulation results obtained with the OPAS method. Statistical uncertainties of the OPAS simulation results are within symbol size. In the right panel, the open squares show simulation results using the same molecular models, but obtained from sampling the chemical potential with thermodynamic integration. Dotted lines show a simultaneous fit to the OPAS simulation results for the activity coefficients of both components using an NRTL model.

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