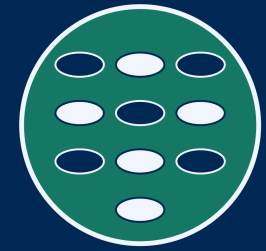




Norges miljø- og
biovitenskapelige
universitet

Materialteori og -informatikk

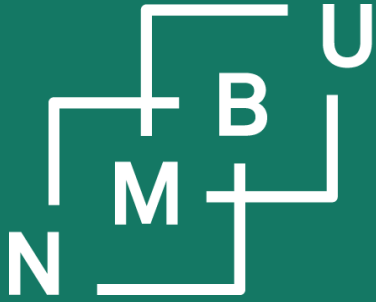


Digitalisering på Ås

Virial and test transformation methods for the spherical surface tension: Statistical mechanical consistency and thermodynamic validity

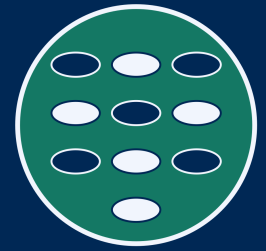
Martin Thomas Horsch
Norwegian University of Life Sciences

28th January 2025, UKRI STFC Daresbury Laboratory
CECAM Workshop on Interfacial Properties: Open Questions (IPOQ 2025)



Noregs miljø- og
biovitenskaplege
universitet

Materialteori og -informatikk



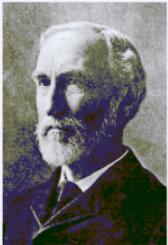
Digitalisering på Ås

1. Background and motivation
2. *Statistical mechanical perspective*
3. *Thermodynamic perspective*
4. *Interfacial properties: Open questions*

Gibbs' interfacial thermodynamics

Two-phase system: Total differential for the Helmholtz free energy

$$dF = \boldsymbol{\mu} d\mathbf{N} - p' dV' - p'' dV'' - S dT + \gamma da.$$



„take some point [...] and **imagine a geometrical surface** to pass through this point and all other points which are similarly situated [...] called the dividing surface“.¹

¹J. W. Gibbs, *Transact. CT Acad. Arts Sci.* 3, 343 – 524, **1878**.

Thermodynamic **excess quantities** are ascribed to this dividing surface:

$$X^{\text{System}} = X' + X'' + X^E.$$

The **dividing surface can be chosen freely**, and the interfacial excess properties (among others) depend on the **notion of the dividing surface**, for which we will use a subscript v .

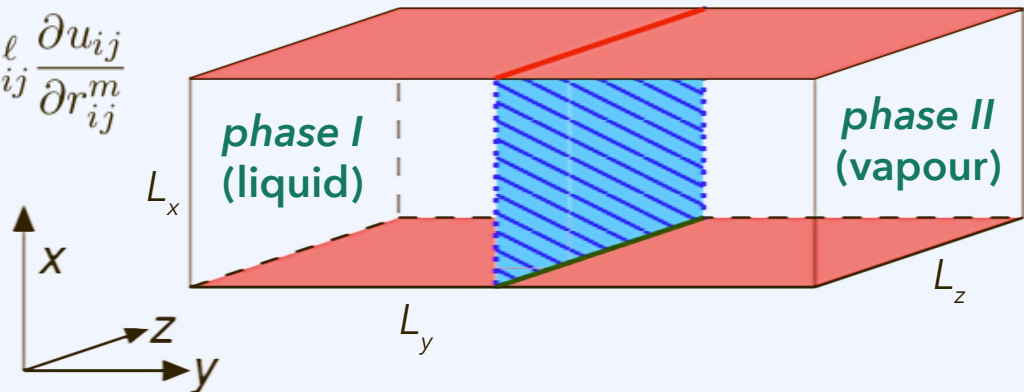
Notation: $\boldsymbol{\mu}$ and \mathbf{N} are vectors (multiple components in the case of a mixture).

Molecular-level observable: The virial

$$\Pi^{\ell m} = \sum_{\{i,j\}} r_{ij}^{\ell} f_{ij}^m = - \sum_{\{i,j\}} r_{ij}^{\ell} \frac{\partial u_{ij}}{\partial r_{ij}^m}$$

Pressure tensor:

$$\mathbf{P} = \mathbf{1}\rho T + \frac{\langle \mathbf{\Pi} \rangle}{V}$$



Planar surface tension:

$$\gamma = (P_n - P_t) L_y$$

$$= \int_0^{L_y} [P_n(y) - P_t(y)] dy$$

planar dividing surface

liquid

vapour

molecule *i*

molecule *j*

tangential

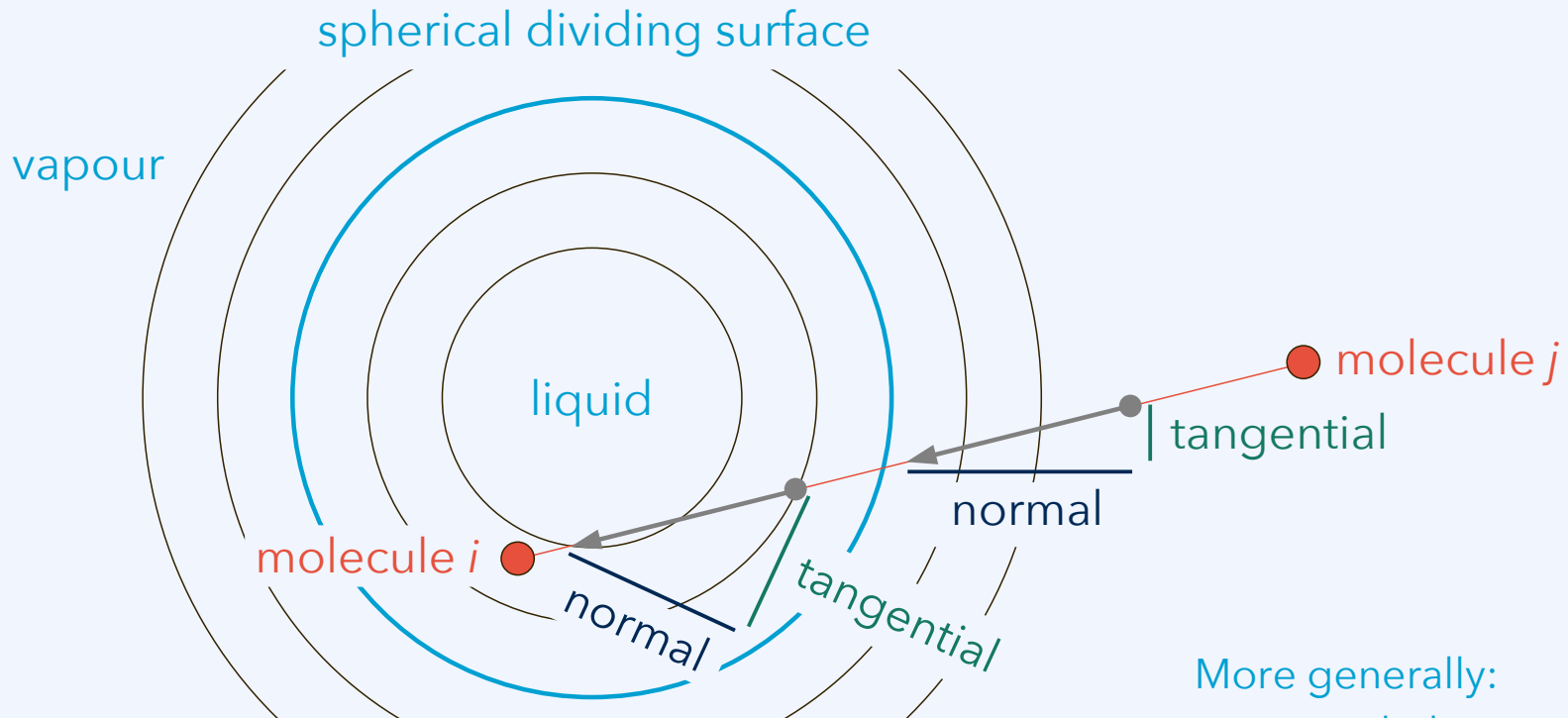
normal

y

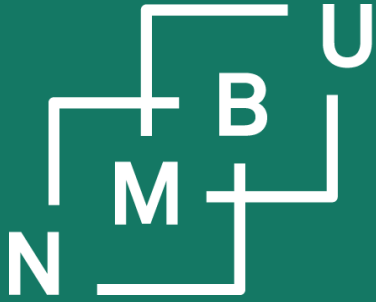
Non-uniqueness in the spherical case

Bakker-Buff equation:
$$\gamma = R^{-2} \int_0^{\infty} (P_n(r) - P_t(r)) r^2 dr$$

The results from this are **not** uniquely defined!

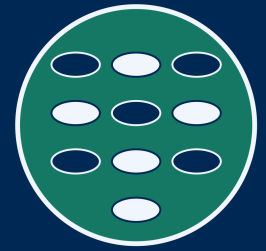


More generally:
Dispersed phase α
Surrounding phase β



Noregs miljø- og
biovitenskaplege
universitet

Materialteori og -informatikk

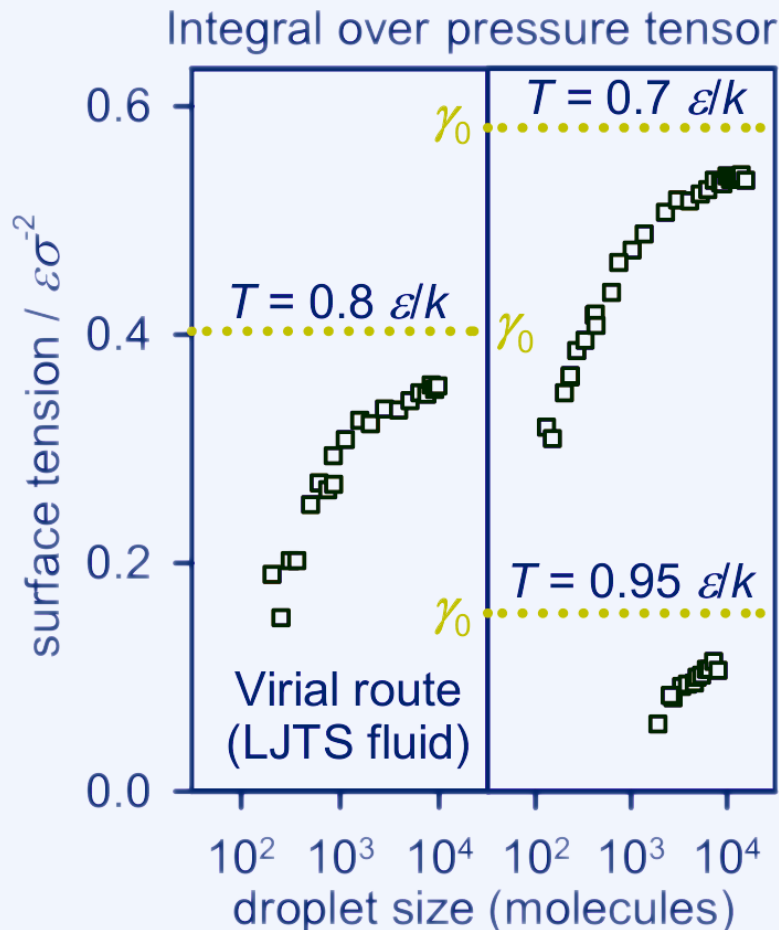


Digitalisering på Ås

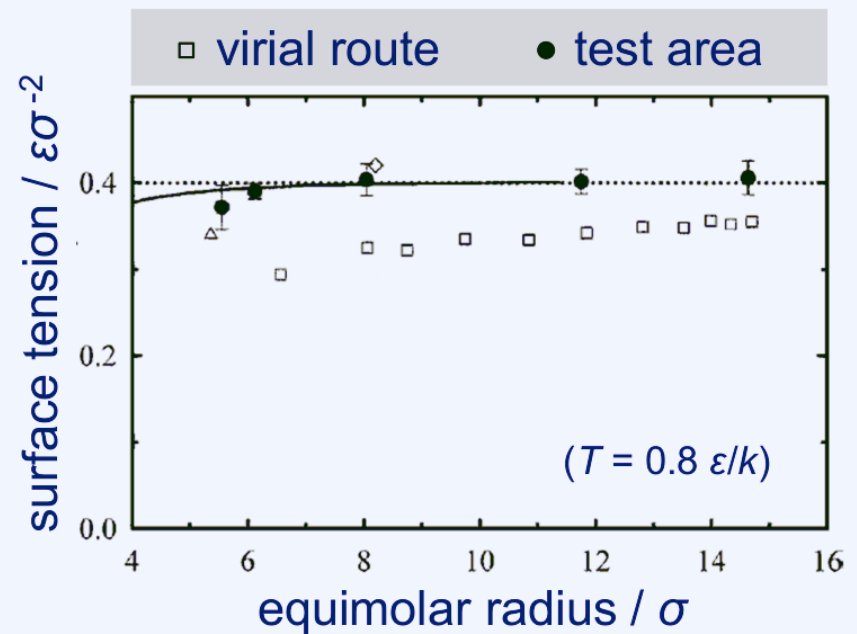
1. Background and motivation
2. Statistical mechanical perspective
3. *Thermodynamic perspective*
4. *Interfacial properties: Open questions*

Virial & test area: Disagreement in the spherical case

Virial route over spherical profiles



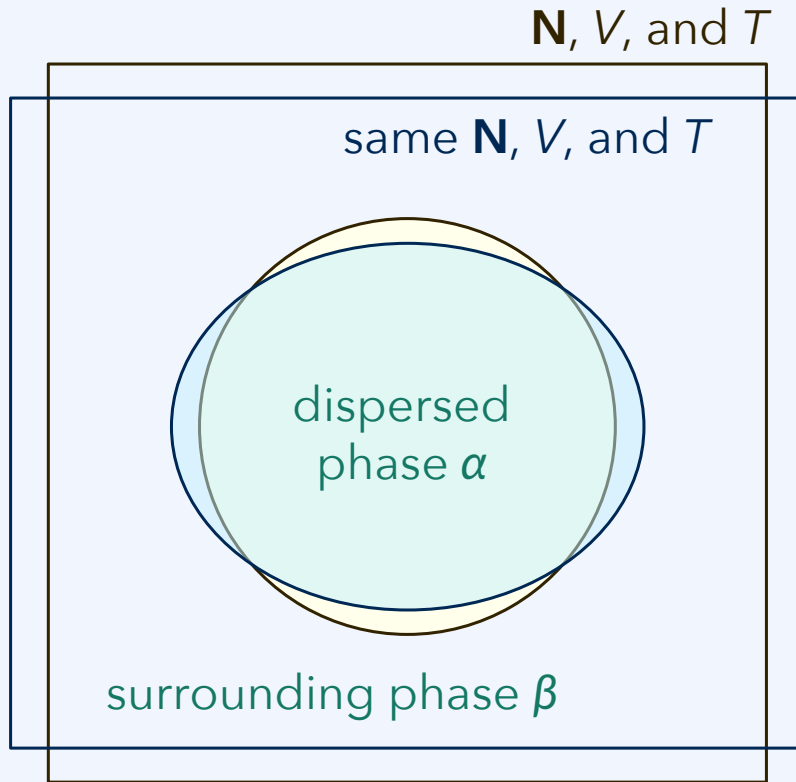
Test area - deformation of the system



Results obtained from the two methods are clearly not in agreement with each other.

Left: Vrabec *et al.*, 2006, Horsch *et al.*, 2008.
Right: Sampayo *et al.*, 2010.

Test area method for spherical geometries^{1, 2}



Test transformation:

$$\mathbf{q}_i \mapsto \Lambda \mathbf{q}_i = \begin{pmatrix} \sqrt{1+\chi} & 0 & 0 \\ 0 & \sqrt{1+\chi} & 0 \\ 0 & 0 & 1/[1+\chi] \end{pmatrix} \mathbf{q}_i$$

Sample ΔF from potential energy change:

$$\Delta F = \underbrace{\langle \Delta U \rangle}_{\Delta F_1, \text{ average } \Delta U} - \frac{1}{2T} \underbrace{\left(\langle \Delta U^2 \rangle - \langle \Delta U \rangle^2 \right)}_{\Delta F_2, \text{ variance of } \Delta U} + \mathcal{O}(\chi^3),$$

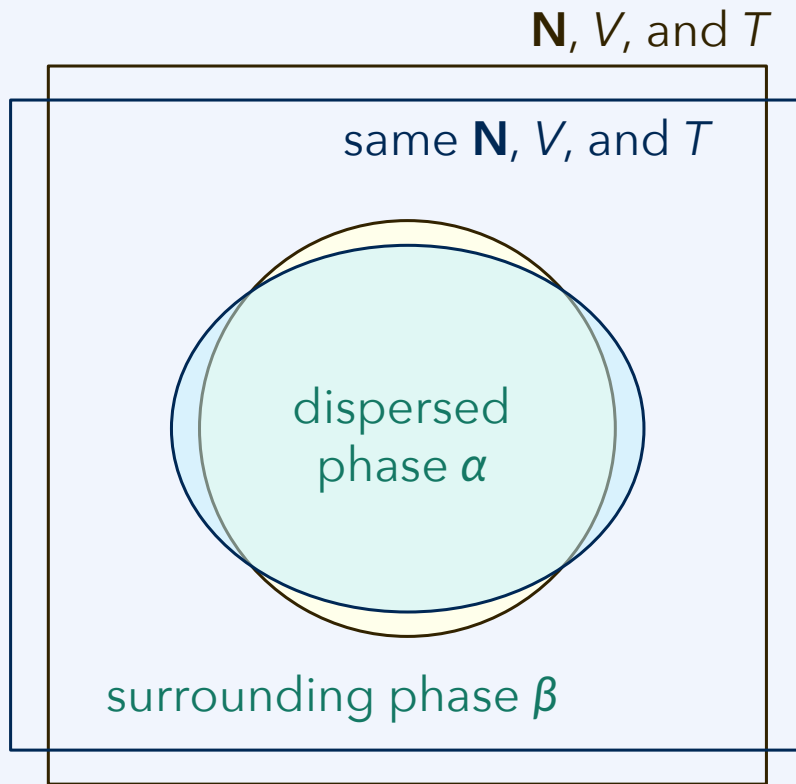
Surface change Δa is proportional to the **square distortion** (different from planar case):

$$\Delta a = \frac{8\pi}{5} R^2 \chi^2 + \mathcal{O}(\chi^3)$$

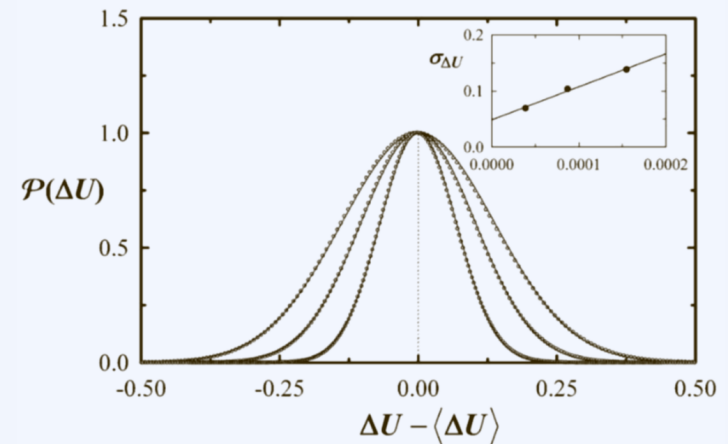
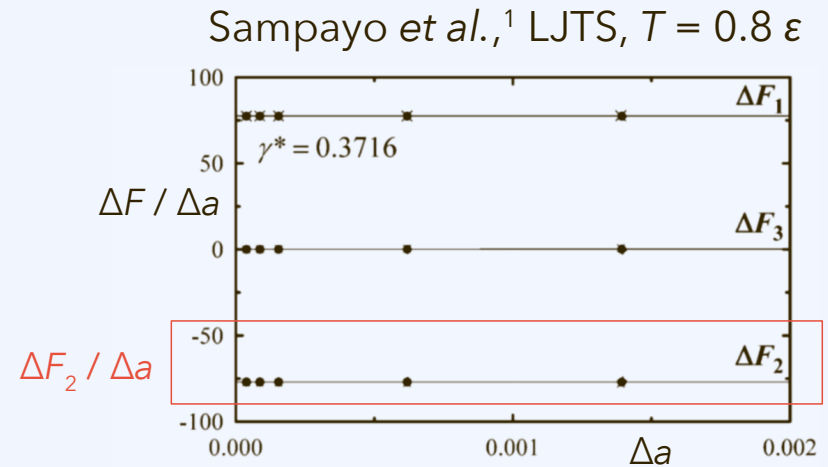
¹J. G. Sampayo, A. Malijevský, *et al.*, *J. Chem. Phys.* **132**: 141101, doi:10.1063/1.3376612, **2010**.

²G. V. Lau, I. J. Ford, *et al.*, *J. Chem. Phys.* **142**: 114701, doi:10.1063/1.4913371, **2015**.

Test area method for spherical geometries^{1,2}



In the planar case, the contribution from ΔF_2 is negligible. **Not so for spheres.**



¹J. G. Sampayo, A. Malijevský, *et al.*, *J. Chem. Phys.* **132**: 141101, doi:10.1063/1.3376612, **2010**.

²G. V. Lau, I. J. Ford, *et al.*, *J. Chem. Phys.* **142**: 114701, doi:10.1063/1.4913371, **2015**.

Virial route in agreement with the test area method

From the planar case, we know: Taking the limit $\chi \rightarrow 0$ for the test area method results in the virial route expression. The two are then in agreement by design.

We can do the same for the spherical case, from expressions by Lau *et al.*:¹

$$\Delta U(\mathbf{q}) = \alpha(\mathbf{q})\chi + \beta(\mathbf{q})\chi^2 + \mathcal{O}(\chi^3)$$

this is the
sampled quantity

This expansion results in:¹

$$\begin{aligned} \Delta F_1 &= \langle \Delta U \rangle = \langle \beta \rangle \chi^2 + \mathcal{O}(\chi^3) \\ \Delta F_2 &= -\frac{\text{Var } \Delta U}{2T} = -\frac{\langle \alpha^2 \rangle}{2T} \chi^2 + \mathcal{O}(\chi^3) \end{aligned}$$

note that the leading contribution is quadratic in χ

$\left(\frac{\partial F}{\partial [\chi^2]} \right)_{\mathbf{N},V,T} = \langle \beta \rangle - \frac{\langle \alpha^2 \rangle}{2T}$

The surface tension is obtained as:¹

$$\gamma = \left(\frac{\partial F}{\partial [\chi^2]} \frac{\partial [\chi^2]}{\partial a} \right)_{\mathbf{N},V,T} = \frac{5 \langle \beta - \alpha^2/2T \rangle}{8\pi R^2}$$

¹G. V. Lau, I. J. Ford, *et al.*, *J. Chem. Phys.* **142**: 114701, doi:10.1063/1.4913371, **2015**.

Virial route in agreement with the test area method

We need to find the corresponding statistical mechanical observables.

For this, we introduce the k -th order virial tensor:

$$\Pi_k^{\ell_1 \dots \ell_{2k}}(\mathbf{q}) = \frac{(-1)^k}{k!} \sum_{\{i,j\}} r_{ij}^{\ell_1} \dots r_{ij}^{\ell_k} \frac{\partial^k u_{ij}}{\partial r_{ij}^{\ell_{k+1}} \dots \partial r_{ij}^{\ell_{2k}}}$$
$$\Pi_k(\mathbf{q}) = \Pi_k^{x \dots x}(\mathbf{q}) + \Pi_k^{y \dots y}(\mathbf{q}) + \Pi_k^{z \dots z}(\mathbf{q})$$

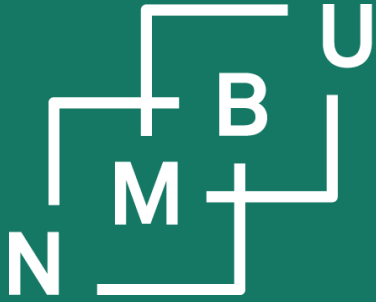
The k -th order virial contains the k -th derivative of the pair potential.

Result: In a molecular simulation, the following would need to be sampled.

$$\langle \alpha^2 \rangle = \frac{1}{2} \langle \Pi_1^2 \rangle - \frac{3}{2} \sum_{\{\ell,m\}} \langle \Pi_1^{\ell\ell} \Pi_1^{mm} \rangle$$
$$\langle \beta \rangle = -\frac{1}{2} \langle \Pi_1 \rangle + \frac{1}{2} \langle \Pi_2 \rangle - \frac{1}{2} \sum_{\{\ell,m\}} \langle \Pi_2^{\ell m \ell m} \rangle$$

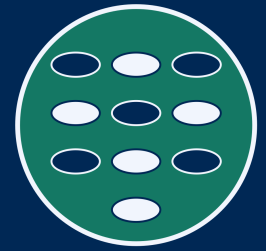
We need the **second-order virial tensor** Π_2 , and hence, the second derivative of $u_{ij}(r_{ij})$.

The pre-existing virial-route methods are wrong because they lack this contribution.



Noregs miljø- og
biovitenskaplege
universitet

Materialteori og -informatikk

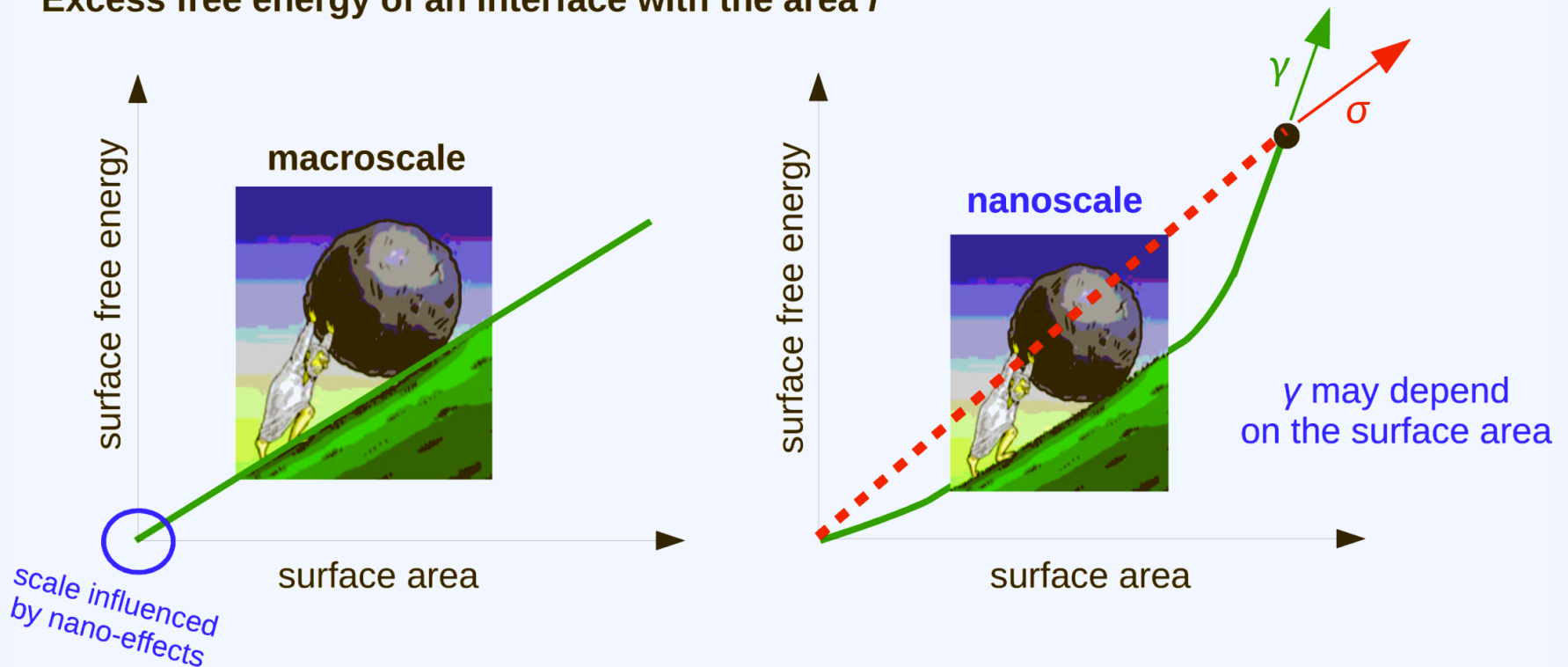


Digitalisering på Ås

1. Background and motivation
2. Statistical mechanical perspective
3. Thermodynamic perspective
4. *Interfacial properties: Open questions*

Definitions of the surface tension

Excess free energy of an interface with the area f



Let us denote **surface tensions** defined as derivatives of a thermodynamic potential by γ , and **surface tensions** defined as absolute excesses by σ .

Definitions of the surface tension

Recall: The notion of the dividing surface ν is represented by subscript indices.

Absolute surface tension $\sigma_\nu = \frac{\Omega_\nu^E}{a_\nu}$

- Used to define the Laplace radius ($\nu = L$), by $\Delta P = 2\sigma_L / R_L$
- Choosing $\nu = L$ means minimizing the absolute surface tension.¹

Total-differential surface tension γ_ν from

$$dF = \mu dN - P^\alpha dV_\nu^\alpha - P^\beta dV_\nu^\beta - S dT + \gamma_\nu da_\nu$$

- The Laplace equation $\Delta P = 2\gamma_\nu / R_\nu$ holds for any ν . Hence, $\gamma_L = \sigma_L$.

¹S. Kondo, *J. Phys. Soc. Jap.* **10**(5): 381–386, doi:10.1143/jpsj.10.381, **1955**.

Definitions of the surface tension

Recall: The notion of the dividing surface ν is represented by subscript indices.

Absolute surface tension $\sigma_\nu = \frac{\Omega_\nu^E}{a_\nu}$

- Used to define the Laplace radius ($\nu = L$), by $\Delta P = 2\sigma_L / R_L$
- Choosing $\nu = L$ means minimizing the absolute surface tension.¹

Total-differential surface tension γ_ν from

$$dF = \mu dN - P^\alpha dV_\nu^\alpha - P^\beta dV_\nu^\beta - S dT + \gamma_\nu da_\nu$$

- The Laplace equation $\Delta P = 2\gamma_\nu / R_\nu$ holds for any ν . Hence, $\gamma_L = \sigma_L$.
- Note that **we may not write** $F(\mathbf{N}, V^\alpha, V^\beta, T, a_\nu)$ or $\gamma_\nu = (\partial F / \partial a_\nu)_{\mathbf{N}, V^\alpha, V^\beta, T}$

Partial-differential surface tension $\hat{\gamma}_\nu^{\mathbb{B}} = \left(\frac{\partial \Omega_\nu^E}{\partial a_\nu} \right)_{\mathbb{B}}$ for a set of variables \mathbb{B} .

- Only well-defined in cases where we can write $\Omega_\nu^E(a_\nu, \mathbb{B})$

¹S. Kondo, *J. Phys. Soc. Jap.* **10**(5): 381–386, doi:10.1143/jpsj.10.381, **1955**.

Gibbs adsorption equation

Compare the total differential

$$d\Omega = -\mathbf{N} d\boldsymbol{\mu} - P^\alpha dV_\nu^\alpha - P^\beta dV_\nu^\beta - S dT + \gamma_\nu da_\nu$$

to the differentiated form of $\Omega = -P^\alpha V_\nu^\alpha - P^\beta V_\nu^\beta + \sigma_\nu a_\nu$.

$$d\Omega = -P^\alpha dV_\nu^\alpha - V_\nu^\alpha dP^\alpha - P^\beta dV_\nu^\beta - V_\nu^\beta dP^\beta + \sigma_\nu da_\nu + a_\nu d\sigma_\nu$$

$$d\Omega = -\mathbf{N} d\boldsymbol{\mu} - P^\alpha dV_\nu^\alpha - P^\beta dV_\nu^\beta - S dT + \gamma_\nu da_\nu$$

$$0 = \mathbf{N} d\boldsymbol{\mu} - V_\nu^\alpha dP^\alpha - V_\nu^\beta dP^\beta + S dT + (\sigma_\nu - \gamma_\nu) da_\nu + a_\nu d\sigma_\nu$$

$$0 = \mathbf{N}_\nu^\alpha d\boldsymbol{\mu} - V_\nu^\alpha dP^\alpha + S_\nu^\alpha dT$$

$$0 = \mathbf{N}_\nu^\beta d\boldsymbol{\mu} - V_\nu^\beta dP^\beta + S_\nu^\beta dT$$

Gibbs-Duhem equation

$$0 = \mathbf{N}_\nu^E d\boldsymbol{\mu} + S_\nu^E dT + (\sigma_\nu - \gamma_\nu) da_\nu + a_\nu d\sigma_\nu$$

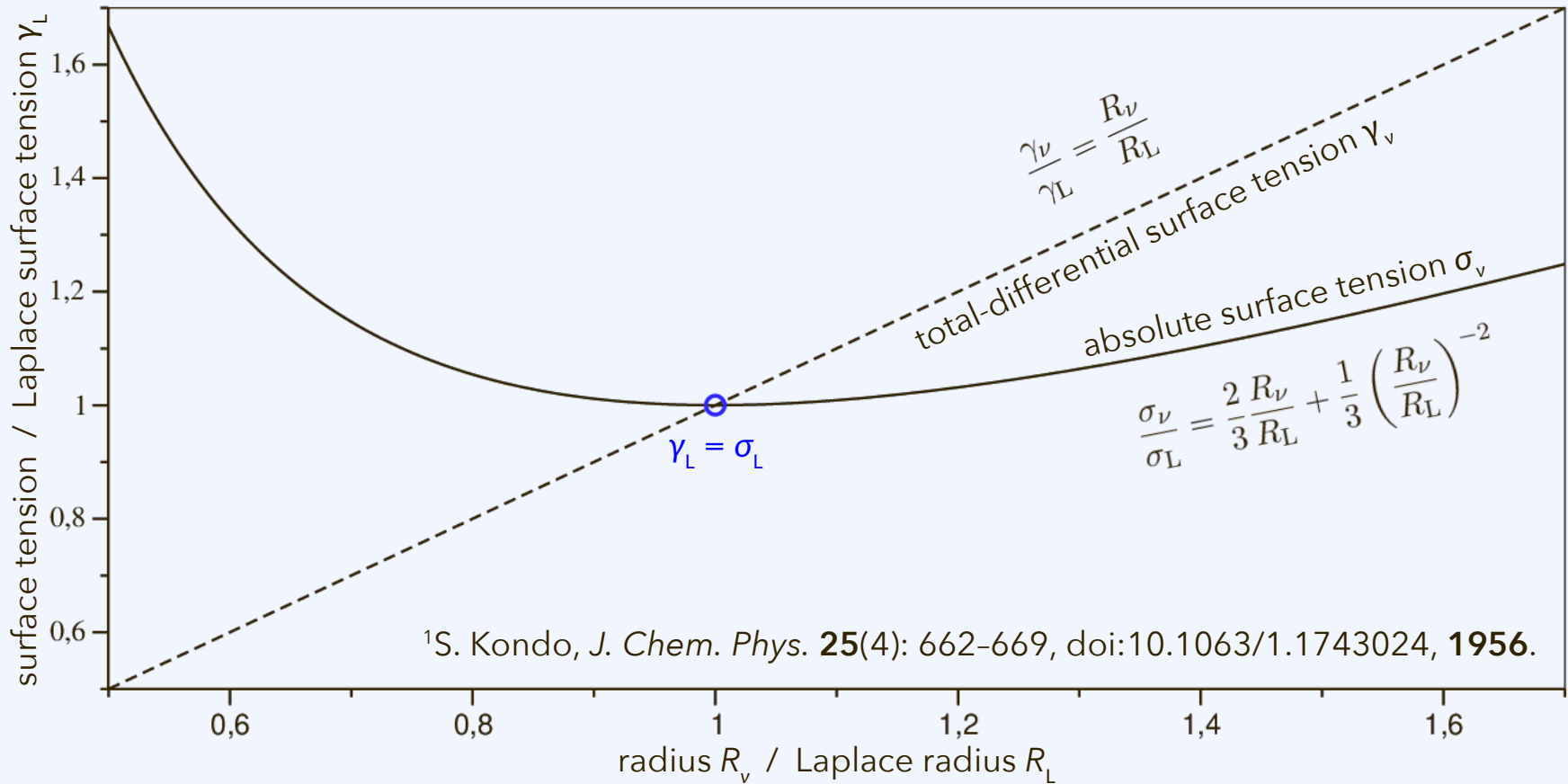
$$\Gamma_\nu = \mathbf{N}_\nu^E / a_\nu$$

$$\zeta_\nu = S_\nu^E / a_\nu$$

$$\gamma_L = \sigma_L$$

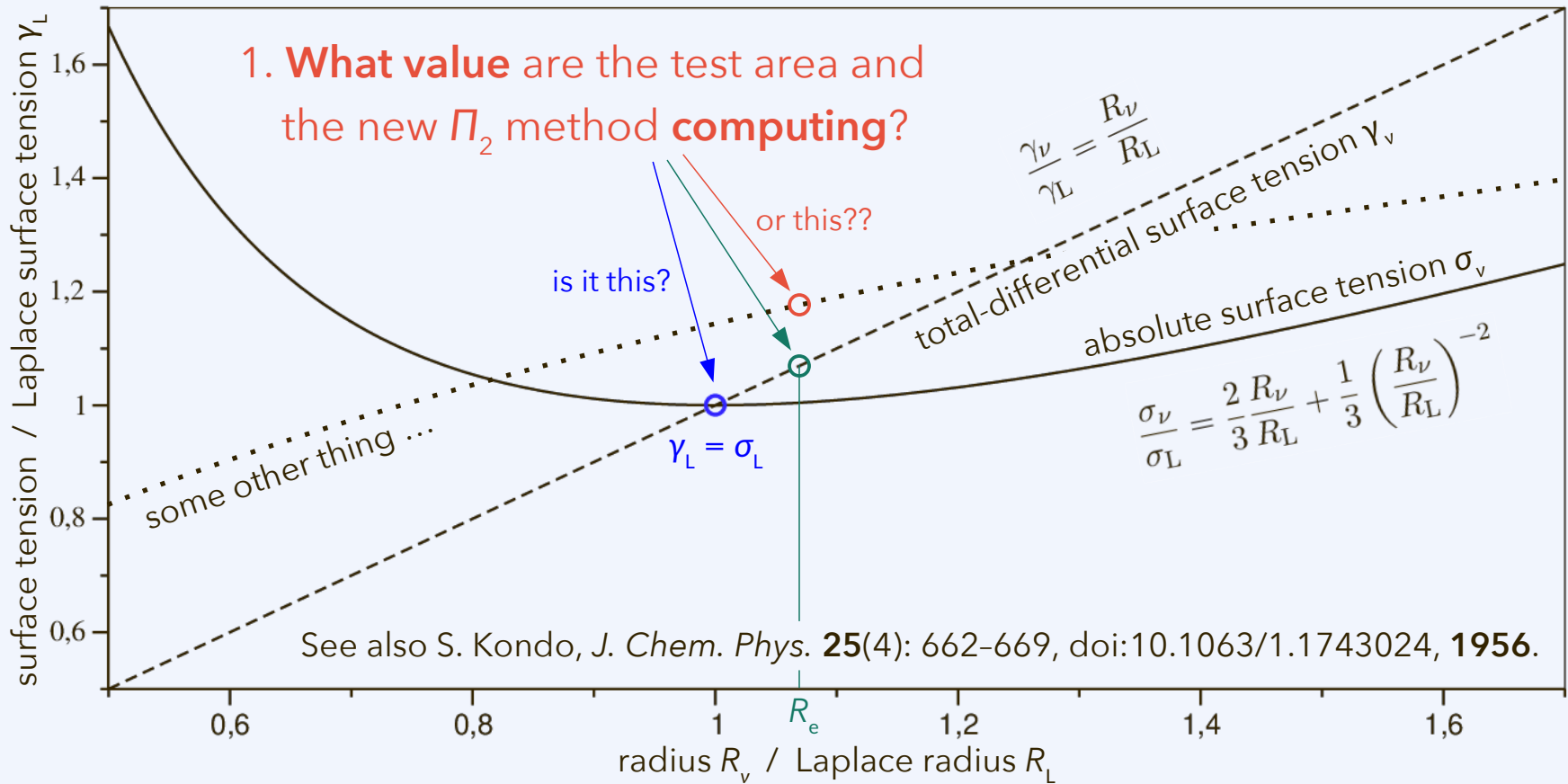
For the Laplace surface, this becomes $d\gamma_L = -\Gamma_L d\boldsymbol{\mu} - \zeta_L dT$.

Absolute vs. total-differential surface tension¹

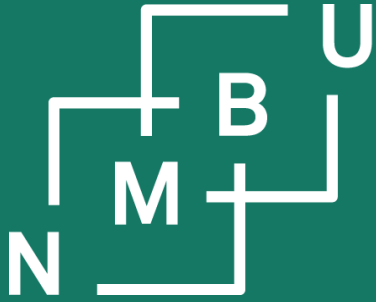


We need to find the [Laplace surface tension](#) and the [Laplace radius](#) to use the [Gibbs adsorption equation](#), [Tolman's law](#), and other [thermodynamic identities](#). A simulation method must allow us to determine them ... *or it is useless*.

This all looks normal - how is it a problem?

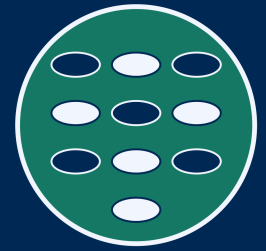


2. We are interested in the **Laplace surface tension** $\gamma_L = \sigma_L$.
3. Our methods are designed to compute a **free energy derivative**.
4. But **I could not figure out how** to express γ_L or σ_L as a free energy derivative.



Noregs miljø- og
biovitenskaplege
universitet

Materialteori og -informatikk



Digitalisering på Ås

1. Background and motivation
2. Statistical mechanical perspective
3. Thermodynamic perspective
4. Interfacial properties: Open questions

Open questions

- 1) It looks like all approaches based on **only the first-order virial** are **necessarily inaccurate**. The proposed **second-order virial** route would **no longer require the ill-defined localized virial** and pressure. But it is not implemented and validated. Once implemented, we can check if it agrees with the TA method.

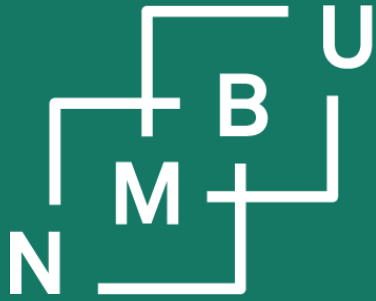
- 2) The **TA method is empirically validated**, its results make sense. It also looks like it is computing some free-energy derivative. But there is **no convincing theoretical grounding** for it, so far. We could attempt describing it as similar to an external field, e.g., based on theory for interfaces in an electric field.

(Suggested name: **Sampayo's demon** - the entity that establishes the distorting field.)

- 3) Maybe the "demon argument" is not needed, and it can still be proven that the TA method in fact computes a **partial-differential surface tension**.

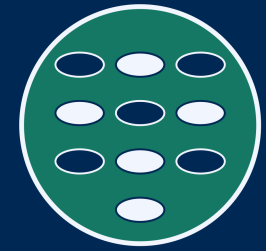
$$\hat{\gamma}_\nu^{\mathbb{B}} = \left(\frac{\partial \Omega_\nu^{\mathbb{E}}}{\partial a_\nu} \right)_{\mathbb{B}}$$

← Could work for $\mathbb{B} = \{\mu, T\}$ with some $\nu \neq L$.
Then it can be proven that this is equal to γ_ν .



Norges miljø- og
biovitenskapelige
universitet

Materialteori og -informatikk



Digitalisering på Ås

Virial and test transformation methods for the spherical surface tension: Statistical mechanical consistency and thermodynamic validity

Martin Thomas Horsch
Norwegian University of Life Sciences

28th January 2025, UKRI STFC Daresbury Laboratory
CECAM Workshop on Interfacial Properties: Open Questions (IPOQ 2025)