# American University of Iraq, Sulaimani Engineering Department Fluid Mechanics, ENGR 356 Term Exam 1

March 11<sup>th</sup>/2018, 6:00-8:00pm Duration 2 hours

Name: -----Student ID: ------

**Instructions:** 

1. Must do questions 1 - 3

2. You are allowed only a basic calculator (not a programmable one)

# 3. Clearly state all your knowns, unknowns, assumptions, and include a basic diagram representing your system.

# Problem 1 (20 marks)

A container with two circular vertical tubes of diameters  $d_1 = 39.5$ mm and  $d_2 = 12.7$ mm is partially filled with mercury. The equilibrium level of the liquid is shown in the left diagram. A cylindrical object made from solid brass is placed in the larger tube (as shown) so that it floats, as shown in the right diagram. The object is D = 37.5mm in diameter and H = 76.2mm high. Calculate the pressure at the lower surface needed to float the object. Determine the new

equilibrium level, *h*, of the mercury with the brass cylinder place. (  $\rho_{water} = i \quad 1000 \quad \frac{kg}{m^3}$  ,

$$g = 9.81 \text{ m/s}^2$$
).



# Problem 2 (20 marks)

At steady state conditions, a pump draws water from a reservoir through a 150-mm diameter suction pipe and delivers it to a 75-mm diameter discharge pipe, as shown on the diagram below. The end of the suction pipe is 2 m below the free surface of the reservoir. The pressure gage on the discharge pipe (2 m above the reservoir face) reads 170 kPa. The average speed in the discharge pipe is 3 m/s. If the pump efficiency is 75 percent, determine the power required to drive it. Effects of pressure, motion and gravity in the reservoir (point 1), as well as Shear and

other work in the entire system are considered negligible.  $\rho_{water} = i + \frac{kg}{m^3}$  and  $g = i + \frac{kg}{m^3}$  and  $g = i + \frac{kg}{m^3}$ 

 $9.81 \text{ m/s}^2$ )



# Problem 3 (20 marks)

A reducer in a piping system is shown. The internal volume of the reducer is 0.2m<sup>3</sup> and its mass is 25kg. Evaluate the total force that must be provided by the surrounding pipes to support the reducer. The fluid flowing through the reducer is gasoline with specific

gravity of 0.72.  $\rho_{water} = i \mod \frac{kg}{m^3}$  and  $g = 9.81 \text{ m/s}^2$ ,  $P_{atm} = 101 \text{ kPa}$ )



# Useful Equations

Definition of specific gravity:	S	$G = \frac{\rho}{\rho_{H_{2}O}}$	(2.3)	Page 23
Definition of specific weight:	$\gamma = \frac{mg}{V} \rightarrow \gamma = \rho g$		(2.4)	Page 23
Definition of streamlines (2D):	$\left(\frac{dy}{dx}\right)_{\text{streamline}} = \frac{v(x, y)}{u(x, y)}$		(2.8)	Page 27
Definition of pathlines (2D):	$\left(\frac{dx}{dt}\right)_{\text{particle}} = u(x, y)$	$(t) \qquad \frac{dy}{dt}\Big)_{\text{particle}} = v(x, y, t)$	(2.9)	Page 27
Definition of streaklines (2D):	$x_{\text{streakine}}(t_0) = x(t, x_0, y_0)$	$(t_0)$ $y_{st makline}(t_0) = y(t, x_0, y_0, t_0)$	( <b>2.10</b> )	Page 27
Newton's law of viscosity (1D flow):	7	$r_{yx} = \mu \frac{du}{dy}$	(2.15)	Page 33
Shear stress for a non-Newtonian fluid (1D flow):	$\tau_{yx} = k \left  \frac{du}{dy} \right ^{n-1} \frac{du}{dy} = \eta \frac{du}{dy}$		(2.17)	Page 35
Hydrostatic pressure variation:	ydrostatic pressure variation: $\frac{dp}{dz} = -\rho g \equiv -\gamma$		(3.6)	Page 59
Hydrostatic pressure variation (incompressible fluid):		$p - p_0 = \Delta p = \rho g h$	(3.7)	Page 61
Hydrostatic pressure variation (several incompressible fluids):		$\Delta p = g \sum_{i} \rho_{i} h_{i}$	(3.8)	Page 65
Hydrostatic force on submerged plane (integral form):		$F_R = \int_A p dA$	(3.10a)	Page 70
Hydrostatic force on submerged plane: $F_R = p_c A$		(3.10b)	Page 70	
Horizontal and vertical hydrostatic forces on curved submerged surface:		$F_H = pcA$ and $F_V = \rho g \Psi$	(3.15)	Page 77
Buoyancy force on submerged object:		$F_{buoyancy} = \rho g V$	(3.16)	Page 80

Continuity (mass conservation), incompressible fluid:	$\int_{\rm CS} \vec{V} \cdot d\vec{A} = 0$	(4.13a)	Page 9
Continuity (mass conservation), incompressible fluid, uniform flow:	$\sum_{\rm CS} \vec{V} \cdot \vec{A} = 0$	(4.13b)	Page
Continuity (mass conservation), steady flow:	$\int_{\rm CS} \rho \vec{V} \cdot d\vec{A} = 0$	(4.15a)	Page
Continuity (mass conservation), steady flow, uniform flow:	$\sum_{\rm CS} \rho \vec{V} \cdot \vec{A} = 0$	(4.15b)	Page
Momentum (Newton's second law):	$\vec{F} = \vec{F}_{S} + \vec{F}_{B} = \frac{\partial}{\partial t} \int_{CV} \vec{V} \rho  d\Psi + \int_{CS} \vec{V} \rho \vec{V} \cdot d\vec{A}$	(4.17a)	Page
Momentum (Newton's second law), uniform flow:	$\vec{F} = \vec{F}_S + \vec{F}_B = \frac{\partial}{\partial t} \int_{CV} \vec{V} \rho  d\Psi + \sum_{CS} \vec{V} \rho  \vec{V} \cdot \vec{A}$	(4.17b)	Page
Momentum (Newton's second law), scalar	$F_x = F_{S_x} + F_{B_x} = \frac{\partial}{\partial t} \int_{CV} u \rho  d\Psi + \int_{CS} u \rho \vec{V} \cdot d\vec{A}$	(4.18a)	Page
components:	$F_{y} = F_{S_{y}} + F_{B_{y}} = \frac{\partial}{\partial t} \int_{CV} v \rho  d\Psi + \int_{CS} v \rho \vec{V} \cdot d\vec{A}$	(4.18b)	
	$F_z = F_{S_z} + F_{B_z} = \frac{\partial}{\partial t} \int_{CV} w \rho  d\Psi + \int_{CS} w \rho \vec{V} \cdot d\vec{A}$	(4.18c)	
Momentum (Newton's second law), uniform flow, scalar	$F_x = F_{S_x} + F_{B_x} = \frac{\partial}{\partial t} \int_{CV} u \rho  d\Psi + \sum_{CS} u \rho \vec{V} \cdot \vec{A}$	(4.18d)	Page
components.	$F_{y} = F_{S_{y}} + F_{B_{y}} = \frac{\partial}{\partial t} \int_{CV} v\rho  d\Psi + \sum_{CS} v  \rho  \vec{V} \cdot \vec{A}$	(4.18e)	
	$F_z = F_{S_z} + F_{B_z} = \frac{\partial}{\partial t} \int_{CV} w \rho  d\Psi + \sum_{CS} w \rho \vec{V} \cdot \vec{A}$	(4.18f)	
Bernoulli equation (steady, incompressible, frictionless, flow along a streamline):	$\frac{p}{\rho} + \frac{V^2}{2} + gz = \text{constant}$	(4.24)	Page
Momentum (Newton's second law), inertial control volume (stationary or constant speed):	$\vec{F} = \vec{F}_S + \vec{F}_B = \frac{\partial}{\partial t} \int_{CV} \vec{V}_{xyz} \rho  d\Psi + \int_{CS} \vec{V}_{xyz} \rho  \vec{V}_{xyz} \cdot d\vec{A}$	(4.26)	Page
Momentum (Newton's second law), rectilinear acceleration of control volume:	$\vec{F_S} + \vec{F_B} - \int_{CV} \vec{a}_{rf} \rho  d\Psi = \frac{\partial}{\partial t} \int_{CV} \vec{V}_{xyz} \rho  d\Psi \int_{CS} \vec{V}_{xyz} \rho \vec{V}_{xyz} \cdot d\vec{A}$	(4.33)	Page
Angular-momentum principle:	$\vec{r} \times \vec{F}_s + \int_{CV} \vec{r} \times \vec{g} \rho d\Psi + \vec{T}_{shaft} = \frac{\partial}{\partial t} \int_{CV} \vec{r} \times \vec{V} \rho d\Psi + \int_{CS} \vec{r} \times \vec{V} \rho \vec{V} \cdot d\vec{A}$	(4.46)	Page
	$\dot{Q} - \dot{W}_s - \dot{W}_{shear} - \dot{W}_{other}$	(4.56)	Page
First law of thermodynamics:	$= \frac{\partial}{\partial t} \int e \rho  d\Psi + \int \left( u + pv + \frac{V^2}{2} + gz \right) \rho \vec{V} \cdot d\vec{A}$		

# **Conversion Factors**

#### Mass and Density

- $\begin{array}{l} 1 \ \text{kg} &= 2.2046 \ \text{lb} \\ 1 \ \text{g/cm}^3 &= 10^3 \ \text{kg/m}^3 \end{array}$
- 1 g/cm<sup>3</sup> = 62.428 lb/ft<sup>3</sup>

- $\begin{array}{l} 1 \ \mbox{lb} &= 0.4536 \ \mbox{kg} \\ 1 \ \mbox{lb/ft}^3 &= 0.016018 \ \mbox{g/cm}^3 \\ 1 \ \mbox{lb/ft}^3 &= 16.018 \ \mbox{kg/m}^3 \end{array}$

#### Length

- 1 cm = 0.3937 in. 1 m = 3.2808 ft
- 1 in. = 2.54 cm
- 1 ft = 0.3048 m

#### Velocity

1 km/h = 0.62137 mile/h 1 mile/h = 1.6093 km/h

# Volume

 $1 \text{ cm}^3 = 0.061024 \text{ in.}^3$  $\begin{array}{rrrr} 1 \ {\rm em} & = \ 0.051024 \ {\rm m} \\ 1 \ {\rm m}^3 & = \ 35.315 \ {\rm ft}^3 \\ 1 \ {\rm L} & = \ 10^{-3} \ {\rm m}^3 \\ 1 \ {\rm L} & = \ 0.0353 \ {\rm ft}^3 \\ 1 \ {\rm m}_{-3}^3 & = \ 16.387 \ {\rm cm}^3 \end{array}$  $1 \text{ ft}^3 = 0.028317 \text{ m}^3$ 1 gal = 0.13368 ft<sup>3</sup>  $1 \text{ gal} = 3.7854 \times 10^{-3} \text{ m}^3$ 

#### Force

- $1 N = 1 kg \cdot m/s^2$ 1 N = 0.22481 lbf1 lbf = 32.174 lb · ft/s2
- 1 lbf = 4.4482 N

#### Pressure

- 1 Pa  $= 1 \text{ N/m}^2$ 
  - $= 1.4504 \times 10^{-4}$  lbf/in.<sup>2</sup>
- $= 10^{5} \text{ N/m}^{2}$ 1 bar
- 1 atm = 1.01325 bar $1 \text{ lbf/in.}^2 = 6894.8 \text{ Pa}$
- $1 \text{ lbf/in.}^2 = 144 \text{ lbf/ft}^2$   $1 \text{ atm} = 14.696 \text{ lbf/in.}^2$

# Energy and Specific Energy

- $= 1 \text{ N} \cdot \text{m} = 0.73756 \text{ ft} \cdot \text{lbf}$ 1 J
- 1 kJ = 737.56 ft · lbf
- = 0.9478 Btu 1 kJ1 kJ/kg = 0.42992 Btu/lb
- $1 \text{ ft} \cdot \text{lbf} = 1.35582 \text{ J}$
- 1 Btu = 778.17 ft lbf
- 1 Btu = 1.0551 kJ
- 1 Btu/lb = 2.326 kJ/kg
- 1 kcal = 4.1868 kJ

## Energy Transfer Rate

1 Btu/h = 0.293 W1 hp = 2545 Btu/h = 550 ft • lbf/s 1 hp = 0.7457 kW1 hp

#### Specific Heat

 $1 \text{ Btu/h} \cdot \circ \mathbf{R} = 4.1868 \text{ kJ/kg} \cdot \mathbf{K}$ 

#### Others

1 ton of refrigeration = 200 Btu/min = 211 kJ/min 1 volt = 1 watt per ampere

# Constants

## Universal Gas Constant

 $\overline{R} = \begin{cases} 8.314 \text{ kJ/kmol} \cdot \text{K} \\ 1545 \text{ ft} \cdot \text{lbf/lbmol} \cdot ^{\circ}\text{R} \\ 1.986 \text{ Btu/lbmol} \cdot ^{\circ}\text{R} \end{cases}$ 

## Standard Acceleration of Gravity

 $g = \begin{cases} 9.80665 \text{ m/s}^2 \\ 32.174 \text{ ft/s}^2 \end{cases}$ 

# Standard Atmospheric Pressure

1.01325 bar 1 atm = { 14.696 lbf/in.2 760 mm Hg = 29.92 in. Hg

#### Temperature Relations

 $T(^{\circ}R) = 1.8 T(K)$  $T(^{\circ}C) = T(K) - 273.15$  $T(^{\circ}F) = T(^{\circ}R) - 459.67$